



RESEARCH ARTICLE

Ionospheric correction of S-band tracking radar data using NavIC S-band signals in missile test range applications

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Abstract

In missile test ranges, complex missions demand precise trajectory generated by radar. Both the radar and Global Navigation Satellite System (GNSS) signals are affected by atmospheric effects, degrading their accuracy and performance. The Indian Regional Navigation Satellite System/Navigation with Indian Constellation (IRNSS/NavIC) transmits signals in the S-band together with the L-band. This paper presents a novel experimental technique to improve the tracking accuracy of S-band radars using the concurrent NavIC S-band signal. The ionospheric delay using the NavIC S-band signal is calculated first, and the results are used to improve the trajectory data of simultaneously operating S-band radars. This is a unique application of the NavIC S-band signals apart from its conventional usage. During a launch mission, for low elevation angles, the ionospheric error is found to be ~ 130 m while at higher elevation angles the error values are found to be ~ 1 – 3 m. The concept is validated using data from a missile test mission. This report on the use of S-band GNSS signals for the correction of S-band radar range data offers a clear advantage of simplicity and accuracy.

1. Introduction

In a missile test range, multiple radars operating in different frequencies are deployed to provide the trajectory information of the flight vehicles under test. In modern scenarios, various types of intermediate-range ballistic missiles (IRBM), inter-continental ballistic missiles (ICBM), cruise missiles, and anti-satellite missile flight experiments are conducted from test ranges, and these exercises demand precise trajectory generation by the tracking radars. The tracking radars calculate the range of the targets based on the rectilinear propagation of the radar waves in free space.

Depending on the operating frequency of the radars and the class of the missile being tracked, the radar data suffers from various kinds of errors due to atmospheric effects on the electromagnetic signals used by the radar. These errors are mainly categorised as ionospheric delay and tropospheric error. Refraction of the radar signals in the troposphere depends on the elevation angle of the radar antenna and the prevailing meteorological conditions. Some studies on tropospheric refraction for C-band tracking radars have been presented (Varaprasad et al., 2012), and the results can also be extended in the case of the S-band operation. For the S-band tracking radars, in addition to the tropospheric error, the contribution of ionospheric delay is also prominent, and it should be considered with importance as it affects the target range calculations in real time.

The ionosphere is a layer of charged particles that stretches from approximately 45 km to 965 km from the surface of the Earth and is characterised by the total electron content (TEC) value (Datta-Barua

et al., 2003; NASA, 2020). TEC has diurnal and seasonal variations due to several factors directly affecting the kinematic density of the electrons in the layer. The actual value of TEC calculated from any point on the surface of the Earth depends on geographical location, local time, season, and associated solar and magnetic activities (Teunissen and Montenbruck, 2017). Standard models, e.g., Klobuchar (Klobuchar, 1987, 1996), global ionosphere map (GIM) (Mannucci et al., 1998), GRAPHIC (Misra and Enge, 2006), GIVE (Dasgupta et al., 2007), NeQuick (Nava et al., 2008), WARTEK (Andrei et al., 2009), Petrie (Petrie et al., 2011), etc. help to theoretically predict the TEC values to a reasonably good accuracy, and therefore can be utilised for the ionospheric delay calculations. These models are used for the signals from satellite-based navigation systems generally transmitting the signal in the L-band of radio frequency signals. The models have their relative merits and demerits and have varying accuracies at different geographical locations. Extensive research to calculate the ionospheric delay in S- and C-bands was done for radars during the pre-GNSS era using meteorological parameters (Schmid, 1966). However, these calculations are complex, predictive, and do not use the information on the status of the ionosphere during the time of launch of missiles and hence were not very fruitful. Hunt first used the GNSS signals in the L-band to calculate the TEC (Hunt et al., 2000) and combined TEC values, and refined the data using dual frequency radars (Hunt et al., 2012) for the prediction of ionospheric error for radars in the test range. The models provide a theoretical prediction of associated delays for the S-band tracking radar and can be used to correct the trajectory of the missile under test. However, to date, no experimental study has been done to use the GNSS S-band signals directly to calculate the ionosphere error of the radars operating in the S-band.

Currently, multiple satellite-based navigation systems are in operation, both global (GPS, GLONASS, Galileo, and Beidou) and regional (e.g., Navigation with Indian Constellation [NavIC] and Quasi Zenith Satellite System [QZSS]). These systems are generically designated as the Global Navigation Satellite System (GNSS). The use of GNSS for ionospheric monitoring is an established and popular technique (Akala et al., 2011; Goswami et al., 2017); several detailed and very recent reviews of the technique can be found in the literature (Su et al., 2019; Yuan et al., 2020; Jin et al., 2021, 2022). NavIC is a regional satellite-based navigation system designed, deployed, and maintained by the Indian Space Research Organization (ISRO). The NavIC constellation consists of seven satellites placed in high Earth orbits (HEO). Three of these satellites (named NavIC 1C, 1F, 1G) are in geostationary Earth orbit (GEO) and four satellites (named NavIC 1B, 1D, 1E, 1I) are placed in inclined geosynchronous orbit (IGSO) (Department of Space, 2020) as shown in Figure 1. NavIC signals are transmitted in L5 (1176.45 MHz) and S-bands (2492.028 MHz) of the radio frequency (RF) spectrum. Signals from all seven satellites are always received from any point in India excluding an extremely small part in the northeast, where at least six satellites are always visible (Dan et al., 2020). This typical constellation structure of NavIC with satellites placed in HEO offers unique advantages for ionospheric studies (Sharma et al., 2019) from the service region and research has been done on the use of NavIC signals for atmospheric studies (Bhardwaj et al., 2017). NavIC satellites continuously transmit the S-band signal, which is unique for the constellation and is not present in the case of other constellations. Therefore, NavIC presents an exclusive scope for continuous monitoring of the ionosphere using this S-band signal together with the standard L-band-based monitoring in its service area. This unique feature of NavIC S-band signal availability is exploited in this present study. Here the results obtained through the monitoring of NavIC signals are extended to mitigate the effects of the ionosphere on S-band tracking radars in real time to improve the target trajectory predictions experimentally instead of model-based theoretical predictions. Works on ionospheric study have been done exclusively for NavIC by various researchers (Venkata Ratnam et al., 2018; Desai and Shah, 2019, 2020; Bhardwaj et al., 2020; Dey et al., 2021) but they were primarily restricted to ionospheric research. This research paper is based on the results of experiments using the S-band NavIC signal for real-time improvement of S-band tracking radar performance in a missile test range.

In this paper, we investigate the potential of the S-band NavIC data collected from a missile test range situated at Chandipur, Odisha, India, using conventional methods to calculate the TEC from the location, and to use the results in computing the associated ionospheric delay for the S-band tracking

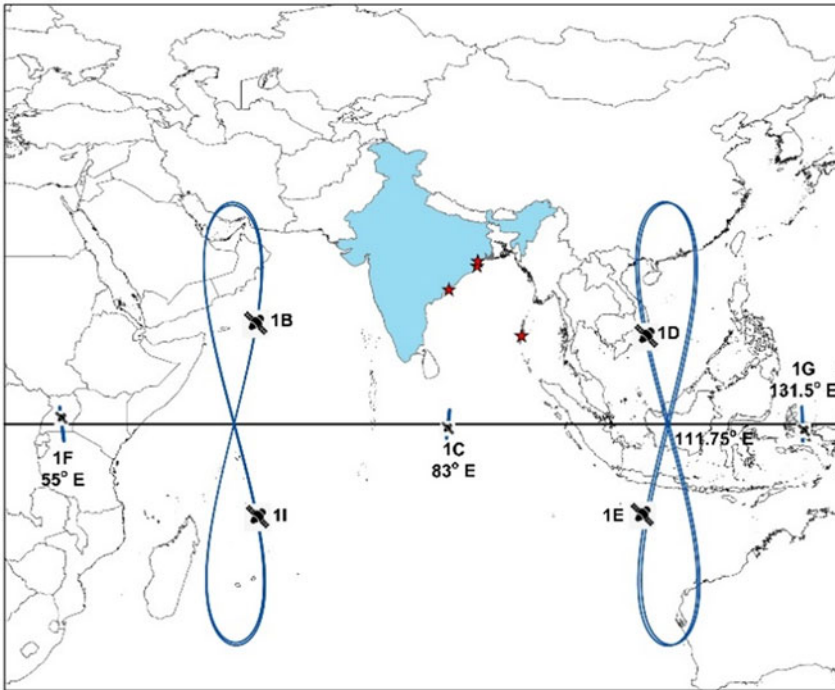


Figure 1. S-band radar locations (brown stars) and NavIC satellite footprints.

radars for improvement of the real-time tracking accuracy. The applicability of the method is typically suitable for the flight azimuth angles of the ballistic and anti-satellite missiles launched from the test range, as these coincide with the azimuthal look angle of the geostationary NavIC 1C satellite. This typical situation offers the benefit of a similar ionospheric pierce point (IPP) location both for the NavIC satellite and for the tracking radar signals, as shown in Figure 2. The flight azimuth directions of the missiles launched from this test range towards the Indian Ocean are also shown in the figure. NavIC 1C is a geostationary satellite; therefore, the corresponding IPP from Chandipur remains approximately fixed. This fixed IPP location is closer to that of the radar under consideration in comparison with the other NavIC GEO satellites, and therefore the S-band signal from the NavIC 1C satellite is considered for this study. The present work shows that the results of ionospheric probing by the NavIC S-band signal of satellite 1C at the test range from satellite 1C can be conveniently used for the improvement of the real-time missile trajectory estimation by the S-band radar at the site.

2. Effect of ionosphere on S-band radar signal

The ionosphere is a dispersive medium for RF waves and the refractive index of the medium is a function of the frequency. The refractive indices are also functions of the electron density of the medium, and the Earth’s magnetic field. RF signals undergo group delay as they pass through the ionosphere and the signals experience significant refraction. The delay of the signal depends on the number of free electrons present along its path. This results in a delay for the pseudo-range (increased value) and an ionospheric phase advance for carrier phase measurements (decreased value) (Teunissen and Montenbruck, 2017).

As per International Telecommunication Union recommendations (ITU Recommendation, 2013), the ionospheric group delay is expressed as

$$t = \frac{1 \cdot 345N_T}{f^2} \times 10^{-7} \tag{1}$$

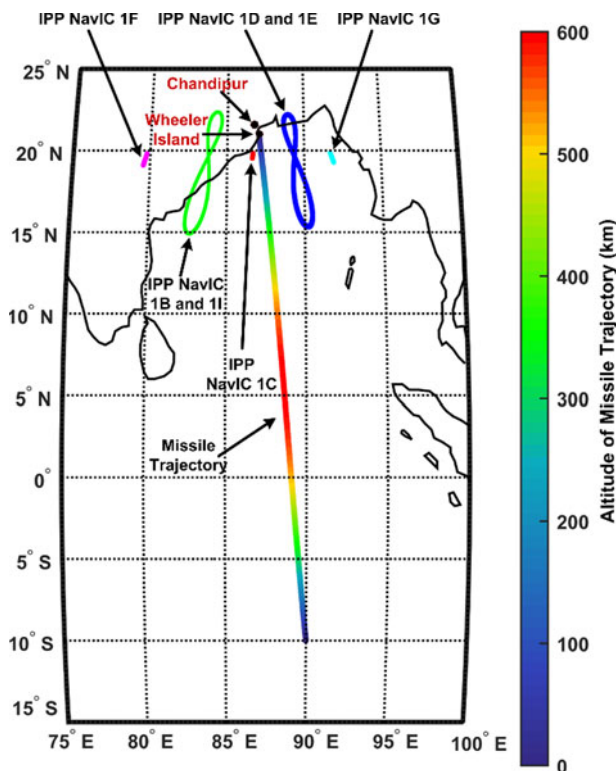


Figure 2. NavIC IPP with respect to the test range location and missile flight azimuth.

In the case of radar, f denotes the tracking radar frequency, and N_T denotes the TEC (electrons per square metre). The group delay can be expressed in metres by multiplying by the speed of light, i.e., by 3×10^8 m/s, and we obtain the equation shown below, which is also used by Hunt et al. (2000).

$$\Delta L = \frac{40 \cdot 3 \int_0^l n_e dl}{f^2} \tag{2}$$

where l represents the one-way signal path length, and n_e is the electron density along the path of the electromagnetic signal, integrated from the target to the radar antenna phase centre. More precisely, n_e is called slant TEC_s, which represents the total number of electrons in a cylindrical column of length l and unit cross-section (1 m²), and it is measured in the unit of 10¹⁶ electrons per square metre. A two-dimensional ionospheric single-layer model is used (Petrie et al., 2011) to convert the slant TEC values (TEC_s) to vertical TEC values (TEC_v) using a simple mapping function. The model assumes that the ionosphere is compressed into a thin shell at the peak ionospheric height of 350 km as shown in Figure 3. The height of the thin shell is taken as the altitude of the IPP and is calculated as described by (Sharma et al., 2019). The collocated radar and NavIC receiver are shown as ‘station’ in the figure, the ‘source’ is the missile under test which is aligned with the direction of the NavIC 1C geostationary satellite.

For any observation location, the TEC through a particular IPP is obtained as $TEC_v = TEC_s \cos(\alpha')$, where

$$\sin \alpha' = \frac{R_E}{R_E + h_m} \sin \alpha \tag{3}$$

R_E is the mean radius of the Earth and h_m represents the height of the maximum electron density from the surface of the Earth, α and α' are the zenith angles at the observation station and the IPP, respectively. In general, the value of h_m is taken as the height corresponding to the maximum electron density at the

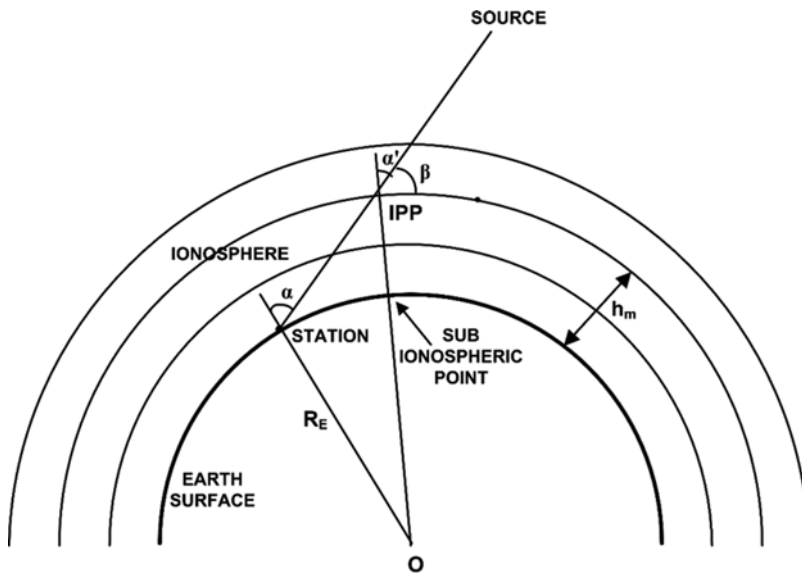


Figure 3. Ionospheric single layer model. (‘Station’ is the location of the radar and the NavIC receiver, ‘Source’ is the instantaneous position of the missile under test that is aligned with the NavIC IC geostationary satellite, ‘IPP’ is the point where the RF signal from the source pierces the ionosphere).

F2 layer peak (Varaprasad et al., 2012). The peak altitude ranges from 250–350 km at middle latitudes and from 350–500 km for location at the equatorial latitude of Chandipur (21 · 43994°N, 87 · 0149° E). Typical values for R_E and h_m at Chandipur are considered to be 6,375 · 3012 km and 450 km respectively on the WGS84 reference ellipsoid (Smith, 1987; Petrie et al., 2011). Now from Equation (2) the one-way group delay of the radar signals while passing through the ionospheric plasma can be expressed as

$$\Delta L = 40 \cdot 3 \sec(\alpha') \text{TEC}_v / f^2 \tag{4}$$

The ionosphere delay (and the TEC) for a particular location can be calculated using different models like GIM, the Klobuchar model, etc. (Klobuchar, 1987, 1996; Mannucci et al., 1998). In this study, TEC is calculated using the ionospheric grid model as this model is used for NavIC (ISRO, 2017).

The objective of the work is achieved in two steps. First, the ionospheric delay in S-band is calculated using the NavIC S-band signal during an active missile test mission in the direction of the missile trajectory from the test range, and then the results are used for the S-band radar signals for different radar antenna elevation angles for correction of missile trajectory estimation. The corresponding methodology and results are presented in the subsequent sections.

3. Correction of tracking radar data using NavIC

The locations of the seven NavIC satellites on the equator or during crossings of the equator are shown in Figure 1, and the IPPs for the NavIC signals from the radar location at Chandipur are shown in Figure 2, together with the missile trajectory. The figures show that the IPP of the NavIC IC satellite is in the same direction as the flight azimuth of the missile path. NavIC IC being a geostationary satellite, the IPP and the look angles (elevation, azimuth) remain almost fixed with regard to the radar location, and therefore the NavIC IC satellite is chosen as the most suitable satellite as the boresight source of S-band signal for calibration of the S-band radar located at Chandipur.

The ionosphere layer has a height of approximately 1,000 km through which the one-way NavIC signal passes while the missiles go up to an altitude of around 800 km. The radar signal tracking the missiles has a two-way journey (transmitted signal and reflected back echo signal) through the

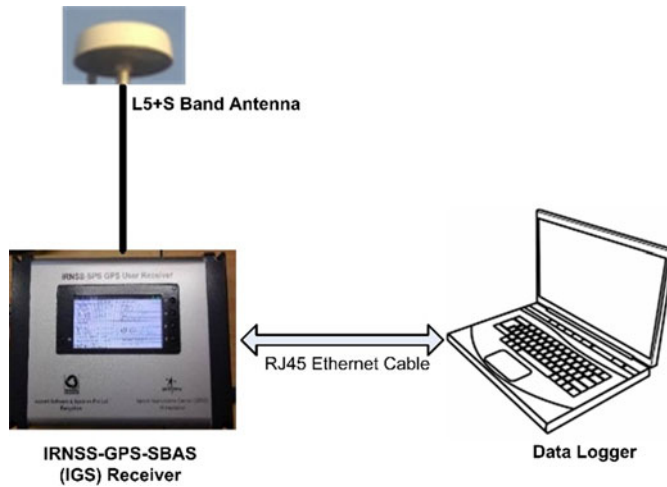


Figure 4. Experimental setup for NavIC S-band data recording at the test range location.

ionosphere and therefore experiences a more prominent effect. Therefore, from a practical viewpoint, the one-way 200 km altitude difference between the missile’s apogee height and the height of the ionosphere as experienced by the NavIC signal is ignored for all practical purposes as it will contribute a negligible error. To begin with, the TEC_v from Chandipur is calculated using NavIC IC data, and then the ionosphere group delay of the signal is calculated corresponding to the radar elevation angles.

3.1. Calculation of TEC at the Chandipur test range site using NavICIC data

The operational frequency of the S-band tracking radar used at the test range is very close to the NavIC S-band signal; a collocated NavIC S-band-enabled GNSS receiver (ISRO IRNSS-GPS-SBAS receiver, ISRO-IGS NavIC Rx) is used to measure the TEC_v and ionospheric delay in S-band.

The ISRO-IGS NavIC receiver with the antenna placed with a clear view of the sky is installed at the test range, as shown in Figure 4. The receiver was operated in NavIC S-band only from 18:30 IST on 26 February 2019 to 10:30 IST on 27 February 2019, which includes the time of an active missile launch mission under consideration. From the raw data provided by the IGS receiver and vendor-supplied data extraction utility, ionosphere delay (iono-delay in metres) is obtained. It is to be noted that the calculated iono-delay is based on the ionosphere grid model and the TEC_s is calculated using Equation (5).

$$TEC_s = \frac{\text{ionosphere delay}}{40 \cdot 3} f_s^2 \text{ el/m}^2 \tag{5}$$

where $f_s = 2492 \cdot 028$ MHz is the NavIC S-band central frequency (ISRO, 2017).

The average elevation angle of the NavIC IC satellite from Chandipur is $64 \cdot 5^\circ$ and therefore the zenith angle is $25 \cdot 5^\circ$. Thus, from Equation (3) we get,

$$\begin{aligned} \sin \alpha' &= \frac{R_e}{R_e + h_m} \sin \alpha = \frac{6375 \cdot 3012}{6375 \cdot 3012 + 450} \sin (90 - 64 \cdot 5^\circ) \\ &= \frac{6375 \cdot 3012}{6375 \cdot 3012 + 450} \cos (64 \cdot 5^\circ) = 0 \cdot 402144749 \end{aligned}$$

and therefore,

$$\alpha' = \sin^{-1}(0 \cdot 402144749) = 23 \cdot 71232574^\circ.$$

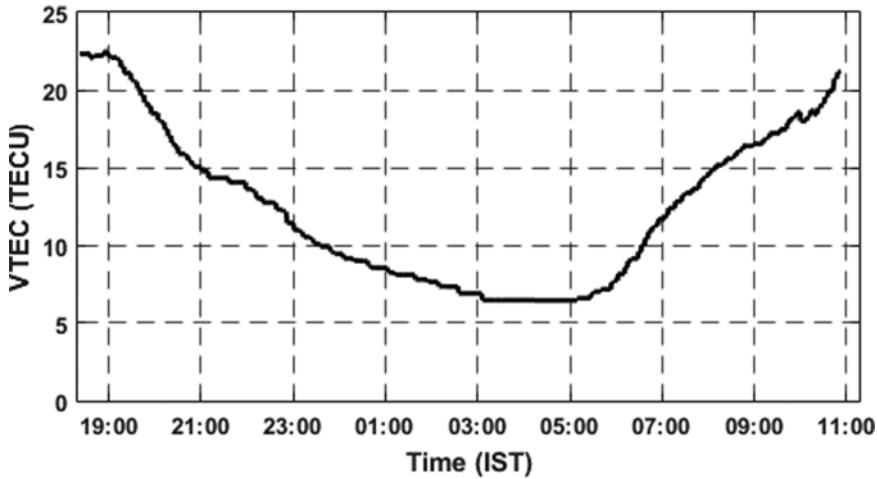


Figure 5. TEC_v variation with time at the test range obtained using NavIC 1C data, $1\text{ TECU} = 10^{16}\text{electrons/m}^2$.

Using Equation (5) the TEC_s values are obtained, and finally, the vertical TEC values are obtained using Equation (6),

$$TEC_v = (TEC_s) \cos \alpha' = TEC_s(0 \cdot 9155761032) \text{ el/m}^2 \tag{6}$$

The TEC_v values at Chandipur for the NavIC 1C satellite are shown against the local time (IST) in Figure 5 as recorded during the night-time launch mission. The TEC_v values range from 7 total electron content unit (TECU) to 23 TECU. As usual, it is observed that TEC is lower during the quiet time before sunrise and becomes higher when the sun is up at the zenith.

3.2. Ionosphere delay variation with the radar elevation angle

Ionosphere delay (ΔL in metres) for different elevation angles of radar is calculated by Equation (4) as $\Delta L = \frac{40 \cdot 3}{(f_{radar})^2} \sec(\theta) TEC_v$, where θ represents the radar zenith angle, f_{radar} represents the radar operating frequency (in Hz). If the radar elevation angle is E_r , then using Equation (6)

$$\begin{aligned} \Delta L &= \frac{40 \cdot 3}{(f_{radar})^2} \sec(90 - E_r) TEC_v \\ &= \frac{40 \cdot 3}{(f_{radar})^2} \text{cosec}(E_r) TEC_s(0 \cdot 9155761032) \\ &= \frac{36 \cdot 897716959}{(f_{radar})^2} \text{cosec}(E_r) TEC_s \end{aligned} \tag{7}$$

If the TEC_s values can be calculated from the NavIC S-band signal from satellite 1C as per Equation (5), then the ΔL values in Equation (7) may be calculated continuously for the tracking radar operating in the same frequency band. Therefore, the results from the NavIC S-band signal monitoring can be directly used to calculate the real-time ionospheric delay for the S-band radars during the actual missile launch, and therefore, for the real-time correction of the target ranges.

Usually, tracking radars in test ranges uses the transponder (or beacon) mode of tracking the missiles. So, there will be two frequencies under consideration, one for the uplink or the transmit frequency, and the other for the downlink from the missile or the receive frequency. Let the frequencies for the transmitted and the received signals from and to the radar be f_{radar_Tx} and f_{radar_Rx} respectively.

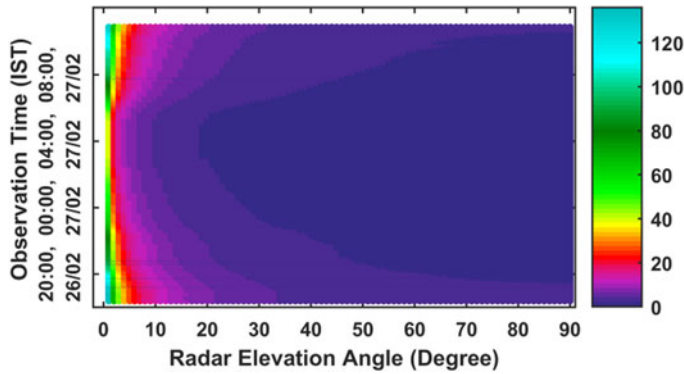


Figure 6. Variation of round-trip ionospheric delay values for the missile trajectory with S-band radar elevation angle calculated using S-band signal from the NavIC 1C satellite. The colour bar on the right side represents different ionosphere delay values (metres).

Then the ionosphere delay during the radar signal transmission is

$$\Delta L_{Tx} = \frac{36 \cdot 897716959}{(f_{radar_Tx})^2} \operatorname{cosec}(E_r) \operatorname{TEC}_s \tag{8}$$

and the ionosphere delay during the reception of the signal is

$$\Delta L_{Rx} = \frac{36 \cdot 897716959}{(f_{radar_Rx})^2} \operatorname{cosec}(E_r) \operatorname{TEC}_s \tag{9}$$

Therefore, the total ionosphere delay during the round-trip signal path during the tracking of the missile is

$$\begin{aligned} \Delta L_{Total} &= \Delta L_{Tx} + \Delta L_{Rx} \\ &= \frac{36 \cdot 897716959}{(f_{radar_Tx})^2} \operatorname{cosec}(E_r) \operatorname{TEC}_s \\ &\quad + \frac{36 \cdot 897716959}{(f_{radar_Rx})^2} \operatorname{cosec}(E_r) \operatorname{TEC}_s \end{aligned} \tag{10}$$

Now, the TEC_s values calculated using the NavIC 1C signal using Equation (6) are used in Equation (10), and the ionosphere group delays corresponding to the radar elevation angles are calculated. The corresponding results are shown in Figure 6 and the expanded view is shown in Figure 7 for better visualisation of the ionosphere error values. A close inspection of Figures 6 and 7 reveals that the ionosphere delay decreases with increasing radar elevation angle E_r . Around 19:00 IST on 26 February 2019, the ionospheric delay saturates beyond 60° elevation angle, during 03:00–05:00 IST, 27 February 2019 beyond the 15° elevation angle the delay saturates. Around 09:00 IST, this delay saturates after a 40° elevation angle. Thus, the time of the missile launch also plays a crucial role in the calculation of the ionospheric delay of the S-band radar signal.

Table 1 depicts the actual round-trip ionospheric delay values for a S-band radar during the observation period of the night-time missile launch mission. It may be seen that, at extremely low elevation angles (1° or 2°), the ionosphere delay goes up to 130 m. At radar elevation angles of between 5° and 10°, the delay varies between 10 and 20 m. At 10°–20° elevation angle, the delay ranges from 5 to 10 m. At 20°–30° elevation angle, the delay ranges between 1 and 3 m, and for 30°–55°, the delay ranges from 1 to 2 m. Above 55° elevation angle, irrespective of time, ionosphere delay saturates approximately at 1.5 m.

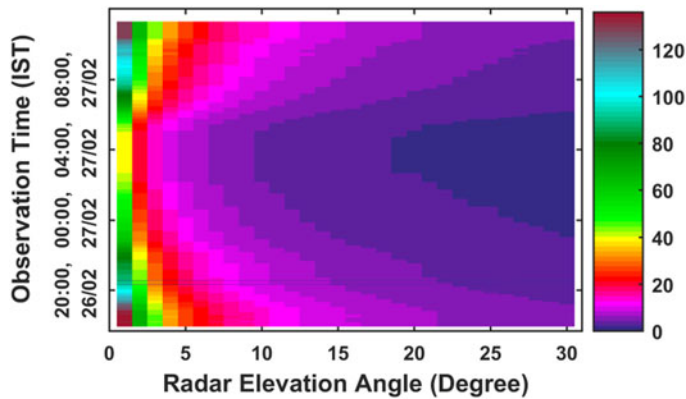


Figure 7. Expanded view for lower S-band radar signal elevation angles. The colour bar on the right side represents different ionosphere delay values (metres).

Table 1. Round-trip ionosphere delay of S-band radar signals as calculated using the S-band signal from NavIC IC at the Chandipur test range location during an active launch mission.

Elevation angle (degrees)	1–2	5–10	10–20	20–30	30–55	>55
Ionosphere delay (m)	130	10–20	5–10	1–3	1–2	1·5

Table 2. Comparison of radar range data for high radar elevation angles.

Time (sec)	INS slant range (SR) (km)	Radar elevation angle (deg)	Radar SR uncorrected (U) (km)	Radar SR corrected (C) (km)	Difference radar SR (U) – INS SR (m)	Difference radar SR – INS SR (C) (m)
208·30	369·59	28·72	370·62	370·61	1025·40	1017·40
210·00	377·30	28·77	378·44	378·43	1139·60	1131·60
211·00	382·05	28·47	383·12	383·11	1062·33	1054·33
212·00	386·67	28·25	387·84	387·83	1162·58	1154·58
213·00	391·54	28·21	392·63	392·62	1090·56	1082·56
214·00	396·27	27·87	397·46	397·45	1195·19	1187·19
215·00	401·25	27·80	402·35	402·34	1101·67	1093·67
216·00	406·09	27·59	407·28	407·27	1193·54	1185·54
217·00	411·09	27·45	412·32	412·31	1231·50	1223·50
218·00	416·25	27·25	417·35	417·34	1108·05	1100·05
219·00	421·26	27·03	422·51	422·50	1247·39	1239·39
220·00	426·54	27·00	427·66	427·65	1118·01	1110·01
221·00	431·68	26·85	432·91	432·90	1235·89	1127·89

The results shown in Table 1 imply that the ionospheric delay values calculated for the observation period using the NavIC S-band signal can be used to improve the accuracy of the S-band tracking radars by incorporating the delay in the final trajectory calculation. Thus, the NavIC S-band signal can provide the elevation angle and time-dependent ionospheric delay values during missile launch periods, which in turn, can be used to improve the real-time range estimation accuracy of the tracking radars. Along

Table 3. Comparison of radar range data for low radar elevation angles.

Time (sec)	INS slant range (SR) (km)	Radar elevation angle (deg)	Radar SR uncorrected (U) (km)	Radar SR corrected (C) (km)	Difference radar SR (U) – INS SR (m)	Difference radar SR – INS SR (C) (m)
573 · 10	2191 · 90	2 · 68	2192 · 29	2192 · 16	396 · 47	226 · 47
573 · 20	2192 · 37	2 · 65	2192 · 87	2192 · 74	504 · 23	374 · 23
573 · 40	2193 · 41	2 · 67	2193 · 66	2193 · 53	248 · 99	118 · 99
573 · 50	2193 · 89	2 · 70	2193 · 95	2193 · 82	62 · 95	–67 · 04
574 · 40	2198 · 06	2 · 67	2198 · 19	2198 · 06	129 · 11	–0 · 88
574 · 50	2198 · 53	2 · 61	2198 · 91	2198 · 78	370 · 81	240 · 81
574 · 60	2199 · 01	2 · 52	2199 · 82	2199 · 69	813 · 45	683 · 45
574 · 70	2199 · 48	2 · 52	2200 · 27	2200 · 14	788 · 65	658 · 65
574 · 80	2199 · 96	2 · 54	2200 · 65	2200 · 52	690 · 04	650 · 04
574 · 90	2200 · 43	2 · 56	2200 · 97	2200 · 84	539 · 48	409 · 48
575 · 00	2200 · 91	2 · 55	2201 · 46	2201 · 33	551 · 13	421 · 13
575 · 10	2201 · 38	2 · 55	2201 · 91	2201 · 78	532 · 74	402 · 74
575 · 20	2201 · 85	2 · 54	2202 · 42	2202 · 29	568 · 11	438 · 11
575 · 30	2202 · 33	2 · 55	2202 · 83	2202 · 70	506 · 54	376 · 54
575 · 40	2202 · 80	2 · 54	2203 · 34	2203 · 21	537 · 04	407 · 04
575 · 50	2203 · 28	2 · 54	2203 · 80	2203 · 67	526 · 89	396 · 89

with the conventional applications, NavIC S-band signals may also be used for strategic purposes where very high real-time accuracy is needed.

The NavIC constellation consists of three geostationary satellites, and therefore, real-time ionospheric correction data may be generated through multiple observation locations that cover a large part of the missile trajectory tested from the Chandipur test range.

To validate the method proposed in this paper, data from a night-time missile test mission are used together with the in-situ NavIC data. Selected portions of the data have been presented in [Table 2](#) for radar high elevation angle and in [Table 3](#) for radar low elevation angle for comparison. Two small parts of the missile trajectory – one at the beginning of the mission with a high elevation angle and the other at a low radar elevation angle – are used here, as shown in [Figures 8 and 9](#). In the figures, the on-board (inertial navigation system) INS-GNSS fused data as received through the telemetry channel from the missile under test is taken as the reference value for the missile slant range; in the figures, the slant ranges obtained from the INS-GNSS, radar elevation angle, the uncorrected slant range from the radar and the corrected radar slant range using S-band NavIC data are shown with regard to the observation time. It is seen in [Figure 8](#) that, during the initial launch phase of around 215 s of tracking, for a slant range of around 400 km and higher radar elevation angles, the correction values are around 8 m as per the proposed method with regard to the reference INS-GNSS data. However, for the time around 575 s with the missile slant range around 2,200 km with very low radar elevation angles around $2 \cdot 5^\circ$, the uncorrected radar slant range data deviates from the INS-GNSS data as shown in [Figure 9](#) and the correction values are calculated to be around 130 m as per the proposed method and the uncorrected radar slant range data is improved to the corrected slant range data. Though the time of travel of the missile in this zone is very short, i.e., for 3–4 s, the analysis is important for correction of the trajectory information as this will improve the target and missile impact point analysis. This experiment validates the applicability of the proposed experimental method for slant range data correction of S-band radars using NavIC signals.

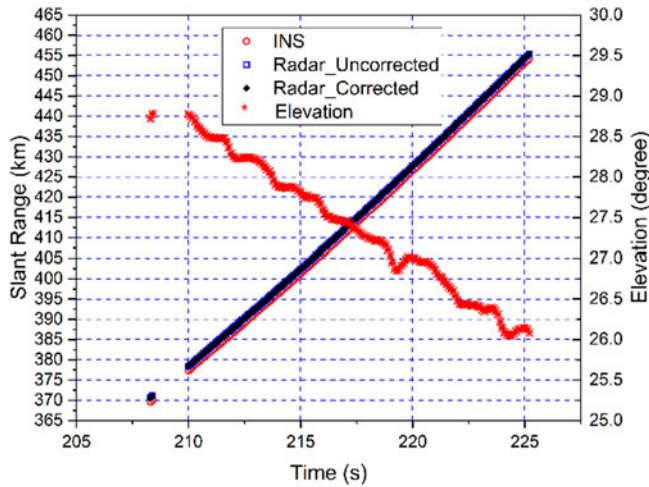


Figure 8. Radar slant range correction using the proposed method for high elevation angles during the initial phase of the mission.

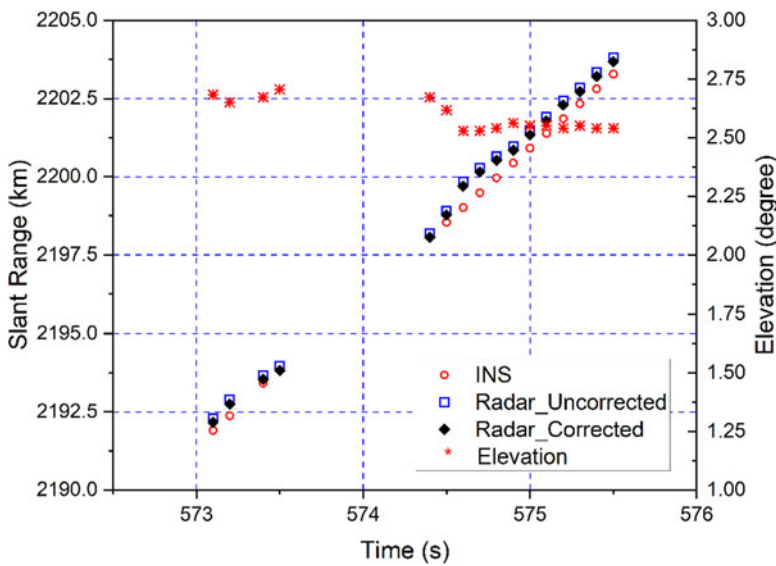


Figure 9. Radar slant range correction using the proposed method for low radar elevation angles during the subsequent phase of the mission.

4. Conclusion

The paper presents a novel experimental approach to improve the real-time tracking accuracy of S-band radar at the Chandipur missile test range by ionospheric delay correction utilising co-located and concurrent NavIC S-band signals. For a particular night-time mission, the associated correction of the radar slant range is shown that validates the proposed method; the method may be extended for any launch mission period. The ionosphere delay decreases as the radar elevation angle increases, and beyond an elevation angle of around 55° the iono-delay values saturate around 1.5 m irrespective of the observation time, but for low radar elevation angles, the error values may be more than 100 m . The results clearly show that the ionospheric delay errors for the tracking radars operating in S-band can

be corrected to improve the measured trajectory of the targets in real time. Depending on the mission-specific target trajectory, the ionospheric delay correction values can be calculated through co-located and simultaneous NavIC S-band observation. Correction of the radar range errors in real time would help in obtaining a more precise trajectory using S-band radars in case of complex missions like missile versus missile ballistic air defence and anti-satellite missions where the actual kinetic kill is of high importance. This may be an important strategic application of NavIC S-band signals beside the conventional position, navigation and timing (PNT) uses.

Future works in this regard would include studies on the ionospheric delay correction of S-band radar signals using concurrent NavIC signal observation from multiple points around the missile launch site, and the use of compact, low-cost S-band enabled NavIC modules for the purpose.

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Competing interests. None.

References

- Akala, A. O., Doherty, P. H., Valladares, C. E., Carrano, C. S. and Sheehan, R. (2011). Statistics of GPS scintillations over South America at three levels of solar activity. *Radio Science*, **46**(5), 1–16. doi: 10.1029/2011rs004678
- Andrei, C. O., Chen, R., Kuusniemi, H., Hernandez-Pajares, M., Juan, J. M. and Salazar, D. (2009). Ionosphere Effect Mitigation for Single-Frequency Precise Point Positioning. *Proceedings of the 22nd International Technical Meeting of the Satellite Division of The Institute of Navigation (ION GNSS 2009)*, 2508–2517.
- Bhardwaj, S. C., Vidyarthi, A., Jassal, B. S. and Shukla, A. K. (2017). Study of Temporal Variation of Vertical TEC Using NavIC Data. *2017 International Conference on Emerging Trends in Computing and Communication Technologies (ICETCCT)*, Dehradun, India. doi:10.1109/ICETCCT.2017.8280317.
- Bhardwaj, S. C., Vidyarthi, A., Jassal, B. S. and Sukla, A. K. (2020). An Assessment of Ionospheric Delay Correction at L5 and S1 Frequencies for NavIC Satellite System. *2020 Global Conference on Wireless and Optical Technologies (GCWOT)*, Malaga, Spain. doi: 10.1109/GCWOT49901.2020.9391601
- Dan, S., Santra, A., Mahato, S. and Bose, A. (2020). NavIC performance over the service region: Availability and solution quality. *Sadhana*, **45**(144), 1–7. doi:10.1007/s12046-020-01375-5
- Dasgupta, A., Paul, A. and Das, A. (2007). Ionospheric total electron (TEC) studies with GPS in the equatorial region. *Indian Journal of Radio and Space Physics*, **36**(4), 278–284.
- Datta-Barua, S., Doherty, P. H., Delay, S. H., Dehel, T. and Klobuchar, J. A. (2003). Ionospheric Scintillation Effects on Single and Dual Frequency GPS Positioning. *Proceedings of ION GPS/GNSS*. Portland, OR: Institute of Navigation, 336–346.
- Department of Space, Indian Space Research Organization. (2020). List of Navigation Satellites. <https://www.isro.gov.in/spacecraft/list-of-navigation-satellites>. Accessed January 2020.
- Desai, M. and Shah, S. (2019). Estimation of ionospheric delay of NavIC/IRNSS signals by using Taylor series expansion. *Journal of Space Weather Space Climate*, **9**, A23. doi:10.1051/swsc/2019023
- Desai, M. and Shah, S. (2020). A local multivariate polynomial regression approach for ionospheric delay estimation of single frequency NavIC receiver. *SN Applied Sciences*, **2**(9), 1–13. doi:10.1007/s42452-020-03250-8
- Dey, A., Joshi, L. M., Chhibba, R. and Sharma, N. (2021). A study of ionospheric effects on IRNSS/NavIC positioning at equatorial latitudes. *Advances in Space Research*, **68**(12), 4872–4883. doi:10.1016/j.asr.2020.09.038
- Goswami, S., Paul, K. S. and Paul, A. (2017). Assessment of GPS multi frequency signal characteristics during periods of ionospheric scintillations from an anomaly crest location. *Radio Science*, **52**(9), 1214–1222. doi:10.1002/2017rs006295
- Hunt, S. M., Close, S., Coster, A. J., Stevens, E., Schuett, L. M. and Vardaro, A. (2000). Equatorial atmospheric and ionospheric modeling at Kwajalein missile range. *Lincoln Laboratory Journal*, **12**(1), 45–64.
- Hunt, S. M., Rich, F. J. and Ginet, G. P. (2012). Ionospheric science at the Reagan test site. *Lincoln Laboratory Journal*, **19**, 89–101.
- ISRO. (2017). *Indian Regional Navigation Satellite System Signal in Space ICD for Standard Positioning Service*. Bangalore: ISRO.
- ITU Recommendation ITU-R 5.531.12. (2013). Ionospheric propagation data and prediction methods required for the design Navan of satellite services and systems.
- Jin, S., Gao, C., Yuan, L., Guo, P., Calabria, A., Ruan, H. and Luo, P. (2021). Long-term variations of plasmaspheric total electron content from topside GPS observations on LEO satellites. *Remote Sensing*, **13**(4), 545. doi:10.3390/rs13040545

- Jin, S., Wang, Q. and Dardanelli, G.** (2022). A review on multi-GNSS for earth observation and emerging applications. *Remote Sensing*, **14**(16), 3930. doi:10.3390/rs14163930
- Klobuchar, J. A.** (1987). Ionospheric time delay algorithm for single frequency GPS users. *IEEE Transactions on Aerospace and Electronic Systems*, **3**, 325–331. doi:10.1109/taes.1987.310829
- Klobuchar, J. A.** (1996). Ionospheric effects on GPS. *Global Positioning System: Theory and Application*. doi:10.2514/5.9781600866388.0485.0515
- Mannucci, A., Wilson, B., Yuan, D., Ho, C., Lindqwister, U. and Runge, T.** (1998). A global mapping technique for GPS-derived ionospheric total electron content measurements. *Radio Science*, **33**(3), 567–582. doi:10.1029/97rs02707
- Misra, P. and Enge, P.** (2006). *Global Positioning Systems: Signals, Measurements and Performance*. 2nd ed. Lincoln, MA: 2006 Ganga-Jamuna Press.
- NASA.** (2020). Earth's Atmospheric Layers https://www.nasa.gov/mission_pages/sunearth/science/atmosphere-layers2.html
- Nava, B., Coisson, P. and Radicella, S. M.** (2008). A new version of the NeQuick ionospheric electron density model. *Journal of Atmospheric and Solar Terrestrial Physics*, **70**(15), 1856–1862. doi:10.1016/j.jastp.2008.01.015
- Petrie, E. J., Hernández-Pajares, M., Spalla, P., Moore, P. and King, M. A.** (2011). A review of higher order ionospheric refraction effects on dual frequency GPS. *Surveys in Geophysics*, **32**(3), 197–253. doi:10.1007/s10712-010-9105-z
- Schmid, P. E.** (1966). *Atmospheric Tracking Errors at S-and C-Band Frequencies*. Washington, DC: National Aeronautics and Space Administration.
- Sharma, A. K., Gurav, O. B., Bose, A., Gaikwad, H. P., Chavan, G. A., Santra, A., Kamble, S. S. and Vhatkar, R. S.** (2019). Potential of IRNSS/NavIC 15 signals for ionospheric studies. *Advances in Space Research*, **63**(10), 3131–3138. doi:10.1016/j.asr.2019.01.029
- Smith, R. W.** (1987). *Department of Defense World Geodetic System 1984: Its Definition and Relationships With Local Geodetic Systems*. Bethesda, USA: Defense Mapping Agency.
- Su, K., Jin, S. and Hoque, M. M.** (2019). Evaluation of ionospheric delay effects on multi-GNSS positioning performance. *Remote Sensing*, **11**(2), 171. doi:10.3390/rs11020171
- Teunissen, P. and Montenbruck, O.** (2017). *Springer Handbook of Global Navigation Satellite Systems*. Springer International Publishing. doi:10.1007/978-3-319-42928-1
- Varaprasad, R., Bhaskara Rao, S. V. and Rao, V. S.** (2012). Effect of troposphere and ionosphere on C-band radar track data and correction of tracking parameters. *Defence Science Journal*, **62**(6), 420–426. doi:10.14429/dsj.62.1160.0
- Venkata Ratnam, D., Raghavendra Vishnu, T. and Sree Harsha, P. B.** (2018). Ionospheric gradients estimation and analysis of S-band navigation signals for NAVIC system. *IEEE Access*, **6**, 66954–66962. doi:10.1109/ACCESS.2018.2876795
- Yuan, L., Jin, S. and Hoque, M.** (2020). Estimation of LEO-GPS receiver differential code bias based on inequality constrained least square and multi-layer mapping function. *GPS Solutions*, **24**(2), 1–12. doi:10.1007/s10291-020-0970-8